Leaching kinetic of Nd, Y, Pr and Sm in rare earth hydroxide (REOH) use nitric acid

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Leaching kinetic of Nd. Y, Pr and Sm in rare earth hydroxide (REOH) use nitric acid

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Abstract. The purpose of this study were to determine the order of reaction, rate reaction constant and activation energy of reaction Y(OH)₃, Nd(OH)₃, Pr(OH)₃ and Sm(OH)₃ with HNO₃. The rate reaction constant is necessary to determine the residence time in the design of continuously stirred tank reactor (CSTR). The studied parameters were leaching temperature (60 – 90 °C) and leaching time (0-15 minutes). From the resulting data can be concluded that the leaching process were strongly influenced by the time and temperature process. Leaching rare earth hydroxide (REOH) using nitric acid follows second order. At leaching 10 grams of REOH using 40 ml HNO₃ 0.0576 mol were obtained maximum conversion at 90 °C and leaching time 15 minutes. For Y was 0.95 (leaching efficiency was 95%), for Nd was 0.97 (leaching efficiency was 97%), for Pr was 0.94 (leaching efficiency was 94%) and for Sm was 0.94 (leaching efficiency was 94%). The largest activation energy was Y of 23.34 kJ /mol followed by Pr of 20.00 kJ /mol, Sm of 17.94 kJ /mol and the smallest was Nd of 16.39 kJ /mol. The relationship between the rate constant of the reaction with T for Y was \( k_Y = 338.26 e^{-23.34/RT} \), for Nd was \( k_{Nd} = 33.69 e^{-16.39/RT} \), for Pr was \( k_{Pr} = 102.04 e^{-20/RT} \) and for Sm adalah \( k_{Sm} = 50.16 e^{-17.94/RT} \)

Keywords: REOH, HNO₃, leaching

1. Introduction

The rare earth elements (REEs) are a unique group of metals regarded as being among the most critical elements that are highly valued for their specialized applications in many modern technologies. In the recent years, REEs have become a significant topic of interest in the metals industry due to a global supply shortage and strengthening demand[1]. This has led many companies to develop processing techniques for extracting REEs from less common rare earth bearing deposits[2] and reclaiming REEs from end-of-life products by recycling (urban mining) spent batteries, phosphors and permanent magnets[3]. One of such examples was the apatite group of minerals (mainly fluorapatite) which are commonly mined for the production of phosphoric acid in the fertilizer industry[4,5,6]. The monazite ores are known to contain significant quantities of REEs and therefore processing of monazite ores for REEs has become more prominent recently[7]. In the processing of monazite deposits however, often require a pre-leach stage prior to the acid bake stage at elevated temperature where the latter converts REE-phosphates to water soluble REE-sulphates[8]. The purpose of the pre-leach stage of the ore / concentrate was to remove the disturbing calcium during the REE manufacturing stage.
Rare earths hydroxide (REOH) was a monazite process products containing REE elements namely Ce, La, Nd, Pr, Y, Sm and Gd[9]. For the separation of each of those elements, REOH should be leached, so that the solution was formed. The leaching reaction that occurs could be between the base with an acid and a base with an acid. The base will react with the acidic solution to form salt and water[10]. K. Stonea et al., who studied comparison of H₃PO₄, HCl, HClO₄ and HNO₃ usage leading to the leaching[11]. Leaching with HNO₃ also for laterite leaching[12]. Use of HNO₃, resulting in the greatest leaching efficiency. In general, leaching of REOH using HNO₃, because in addition of HNO₃ to easy and strong in leaching[13]. Thus Ce will have different properties from other REE elements that have double valences of II and III, so Ce could be separated from other REE elements. Rare earth elements that are easily soluble or are leached are Y, Nd, Pr and Sm while Ce will dissolve later. In this work, REOH was prepared from monazite sand. The leaching of REOH using HNO₃ 0.0576 moles, the parameters were leaching temperature (60 – 90 °C) and leaching time (0-15 minutes). The solution product of leaching are analyzed by XRF.

The purpose of this study were to determine the order of reaction, rate reaction constant and activation energy of reaction Y(OH)₃, Nd(OH)₃, Pr(OH)₃ and Sm(OH)₃ with HNO₃. The rate reaction constant is necessary to determine the residence time in the design of continuously stirred tank reactor (CSTR).

2. Theory
The reaction rate represents the molarity of the solute in the reaction produced each reaction time[14]

\[
A + B \rightarrow C
\]

The reaction rate \( r_A = -\frac{\Delta [A]}{\Delta t} = -\frac{\Delta [B]}{\Delta t} \) (1)

The factors affecting the rate of reaction: temperature, catalyst, molarity and reactant concentration and factors affecting the constant or constant rate of reaction was temperature[15,16,17]. Determination of the constant and leaching reaction rate at the optimum condition of the use of the reactant ratio of REOH with HNO₃. The parameters studied were the variation of leaching time and temperature. The reactions that occurred between REOH and HNO₃ were as follows

\[
\text{RE(OH)}_3(s) + 3\text{HNO}_3(aq) \rightarrow \text{RE(NO}_3)_3(aq) + 3\text{H}_2\text{O}(aq)[18]
\]

s : solid, a : solution
RE : Y, Pr, Nd, Sm

\[ -r_A = k \cdot C_A^n \cdot C_B = (k \cdot C_B) \cdot C_A^n = k \cdot C_A^n \] (3)

n = reaction order
k = the overall reaction rate constant
C_A = concentration (mol) RE
C_B = concentration (mol) HNO₃

In the initial state or \( t_0 \), the number of reagents A or \( N_A \) and at time \( t \) of NA, the conversion of A (\( X_A \)) at a constant volume system was[14]:

\[
X_A = \frac{N_{A0} - N_A}{N_{A0}} = 1 - \frac{C_A}{C_{A0}}
\] (4)
\[ dX_A = \frac{dC_A}{C_{A0}} \] (5)

Data analysis was by integral begins by selecting a certain rate equation to be tested in an integral way and comparing the approximate C-curve relationship with C data to t from the experiment. If they do not match, other estimates are then tested.

**First Order Reaction**

In general, the first order reaction can be represented by the following reaction equation:

\[ A \rightarrow \text{product} \]

If the first order reaction, then the equation of reaction rate was [20]:

\[-r_A = \frac{dC_A}{dt} = kC_A \] (6)

The integration of equation (7) becomes:

\[- \int_{C_{A0}}^{C_A} \frac{dC_A}{C_A} = k \int_{0}^{t} dt \] (7)

\[-\ln \frac{C_A}{C_{A0}} = kt \] (8)

\[ C_{A0} = \text{RE concentration in the feed} \]

\[ C_A = \text{RE concentration after reaction} \]

If expressed in terms of conversion, the equation of rate reaction becomes (9):

\[ \frac{dX_A}{dt} = k(1 - X_A) \] [21]

\[-\ln (1 - X_A) = kt \] [22]

If the graph of the relationship \( \ln (1 - X_A) \) or \( \ln \left( \frac{C_A}{C_{A0}} \right) \) to t was a linear line then the reaction which we observe was correct, following the first order reaction [23].

**Second Order Reaction**

For the second order reaction with the constant rate of reaction referring to the overall reaction rate constant, could use the following equation:

\[ A + 3B \rightarrow C + 3D \]

\[-r_A = -C_{aw}\frac{dX_A}{dt} = -\frac{dC_A}{dt} = kC_A^2 = k(C_{aw} - C_{aw}X_A)(C_{aw} - C_{aw}X_A) \] (11)

\[-r_A = -C_{aw} \frac{dX_A}{dt} = kC_{aw}^2 (1 - X_A)(M - 3X_A) \] (12)

If it was integrated into [24,26,27]

\[ \ln \frac{M - 3X_A}{M(1 - X_A)} = \ln \frac{C_{aw}^2}{C_{aw}^2} = \ln \frac{C_{aw}^2}{M(1 - X_A)k} = \ln \frac{C_{aw}(M - 2kt = (C_{aw} - C_{aw})kt \] (13)

\[ M = \text{comparison (mole B / mol A) start} = \frac{C_{b0}}{C_{a0}} = \text{mole of initial HNO}_3 / \text{mole RE} \]

The experimental variables in equation (13) are made in the form of a \( \ln \left( \frac{M - 3X_A}{M(1 - X_A)} \right) \) vs-t relationship. If a linear line was obtained then the assumption of second order was correct and the \( C_{A0} \) slope (M-2) k. The value of the reaction rate constant was the slope of the linear line divided by \( C_{A0} \) (M-2).

The k relation as a function of temperature by refering to the Arrhenius equation,
\[ k = e^{\frac{E_a}{RT}} \]  
(14)

Han Wang[29], states the relationship between \( k \) and \( T \) was formulated in the equation

\[ \ln k = \ln A - \left( \frac{E_a}{R} \right) \left( \frac{1}{T} \right) \]  
(15)

A was the frequency factor or pre-exponential factor, \( R \) was the universal gas constant = 8.314J / gmol \(^0\)K and \( T \) was the absolute temperature, \(^0\)K, \( E_a \) = activation energy, J / gmole.

The equations for the determination of the reaction order may be used for the reaction of aqueous solids such as Na Thiosulfate with methyl iodide [14] so these equations may be used in the determination of REOH reaction with HNO\(_3\).

3. Methodology

Materials
The materials used were REOH of the processed monazite sand which Ce and La was taken partly (2 times fractionation), technical HNO\(_3\), water, filter paper, Nd\(_2\)O\(_3\), Sm\(_2\)O\(_3\), Pr\(_5\)O\(_{11}\), Y\(_2\)O\(_3\), Merck as analyswas standard materials.

Equipments
Glass equipments, analytic scales, Ikamag heater stirrers, thermometers, ovens, x-ray spectrometers (XRF)

Methods
Nitric acid (HNO\(_3\)) with the molarity of 14.4 M as much as 4 ml was put in the glass beaker added water up to 10 ml plus REOH of 10 grams, heated to a certain temperature of 60 \(^\circ\)C while stirring. The heating time varied 3, 6, 9, 12 and 15 minutes. After each process, the residue was filtered. The leaching solution was taken as 1 ml diluted with water to 5 ml analyzed using XRF. The remaining solids or residues, dried and weighed. The work was repeated for temperatures of 70, 80 and 90 \(^\circ\)C.

Measurable quantities
- The element content (%) in the REOH feed used XRF
- Concentrations of Y, Pr, Nd and Sm (ppm) elements in the leached solution

4. Results and discussion
The results of the composition analysis of REOH (Feed) using XRF were presented in Table 1. In general the largest element content in REOH was Nd, followed by Nd and La. In this research REOH used as the feed was REOH which was partly taken its Ce and La (fractionation 2 times), so that the Nd content increases, La and Ce content decreases.

<table>
<thead>
<tr>
<th>No</th>
<th>Component</th>
<th>Elements concentration %</th>
<th>Atomic Weight</th>
<th>Molecular Weight</th>
<th>Compound Concentration %</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>Y (OH)(_3)</td>
<td>5.36</td>
<td>89</td>
<td>140</td>
<td>8.43</td>
</tr>
<tr>
<td>2</td>
<td>Ce(OH)(_3)</td>
<td>19.07</td>
<td>140</td>
<td>191</td>
<td>26.01</td>
</tr>
<tr>
<td>3</td>
<td>La(OH)(_3)</td>
<td>6.36</td>
<td>139</td>
<td>190</td>
<td>8.69</td>
</tr>
<tr>
<td>4</td>
<td>Nd(OH)(_3)</td>
<td>20.68</td>
<td>144</td>
<td>195</td>
<td>28.00</td>
</tr>
<tr>
<td>5</td>
<td>Sm(OH)(_3)</td>
<td>13.18</td>
<td>150</td>
<td>201</td>
<td>17.66</td>
</tr>
<tr>
<td>6</td>
<td>Pr(OH)(_3)</td>
<td>4.26</td>
<td>141</td>
<td>192</td>
<td>5.80</td>
</tr>
<tr>
<td>7</td>
<td>Dy(OH)(_3)</td>
<td>0.94</td>
<td>162</td>
<td>213</td>
<td>1.24</td>
</tr>
</tbody>
</table>
Effects Temperature and Leaching Time on The Leaching Conversion

From the analysis result of REOH and leaching product solution could be determined or the leaching conversion (X) could be calculated at various time and temperature.

\[
\text{Element conversion (X)} = \frac{\text{weight of element in the feed} - \text{weight of element in the solution}}{\text{weight of element in the feed}} \quad (16)
\]

Weight of element in the feed = concentration of element x weight of REOH
Weight of element in the solution= concentration of element x volume of solution

The effect of time and leaching temperature on the conversion was shown in Figure 1a to Figure 1d. The longer time and the higher leaching temperature, the leaching conversion would be greater. In general reaction, reaction rate one of which was very influenced by temperature and the completely reaction was influenced by reaction time duration.

8  Gd(OH)₃  3.14  157  208  4.16  
  Total  100.00

**Figure 1a.** Correlation between Y leaching time and conversion at various temperature

**Figure 1b.** Correlation between Nd leaching time and conversion at various temperature

**Figure 1c.** Correlation between Pr leaching time and conversion at various temperature

**Figure 1d.** Correlation between Sm leaching time and conversion at various temperature
The conversion value of Y was in the range of 0.00 - 0.95, the Nd conversion values were in the range of 0.00 - 0.97, Pr conversion value were in the range of 0.00 - 0.94 and Sm conversion value were in the range of 0.00 - 0.94.

**Reaction order and rate reaction constant determination**

**First Order Reaction**

In the calculation of reaction rate constant with first order reaction, it was needed the graph of time correlation with \(-\ln (1-X)\) where X was conversion (mole). Based on the equation (13), first order reaction was experimented for finding the reaction constants. The reaction rate was the overall reaction rate constant with the assumption that the concentration of HNO₃ was constant because its amount tends to approach 1, therefore it could be mentioned that the occurring reaction was first order. The calculation results could be seen in Figure 2a to 2d and Table 2.

**Figure 2a.** Correlation between time and \(-\ln(1-X)\) for determining of k value and linearity of first order reaction for Y element

**Figure 2b.** Correlation between time and \(-\ln(1-X)\) for determining k value and linearity of first order reaction for Nd element

**Figure 2c.** Correlation between time and \(-\ln(1-X)\) for determining k value and linearity of first order reaction for Pr element

**Figure 2d.** Correlation between time and \(-\ln(1-X)\) for determining k value and linearity of first order reaction for Sm element
Linear regression values were obtained from square root of $R^2$ of Y, Nd, Pr and Sm elements at various temperature as shown in Table 2.

**Table 2.** The equation and the value of linearity ($R^2$) in the first order reaction

<table>
<thead>
<tr>
<th>Element</th>
<th>Temperature 60 °C</th>
<th>Temperature 70 °C</th>
<th>Temperature 80 °C</th>
<th>Temperature 90 °C</th>
</tr>
</thead>
<tbody>
<tr>
<td>Y</td>
<td>$y_{60} = 0.0835x + 0.394$</td>
<td>$y_{70} = 0.0914x + 0.4322$</td>
<td>$y_{80} = 0.1182x + 0.5317$</td>
<td>$y_{90} = 0.1631x + 0.6384$</td>
</tr>
<tr>
<td></td>
<td>$R^2 = 0.7396$</td>
<td>$R^2 = 0.7557$</td>
<td>$R^2 = 0.7753$</td>
<td>$R^2 = 0.8278$</td>
</tr>
<tr>
<td>Nd</td>
<td>$y_{60} = 0.1061x + 0.4993$</td>
<td>$y_{70} = 0.1139x + 0.5192$</td>
<td>$y_{80} = 0.1425x + 0.5606$</td>
<td>$y_{90} = 0.2152x + 0.7458$</td>
</tr>
<tr>
<td></td>
<td>$R^2 = 0.7675$</td>
<td>$R^2 = 0.778$</td>
<td>$R^2 = 0.8231$</td>
<td>$R^2 = 0.8453$</td>
</tr>
<tr>
<td>Pr</td>
<td>$y_{60} = 0.0886x + 0.4336$</td>
<td>$y_{70} = 0.0886x + 0.4336$</td>
<td>$y_{80} = 0.1056x + 0.4739$</td>
<td>$y_{90} = 0.1485x + 0.5911$</td>
</tr>
<tr>
<td></td>
<td>$R^2 = 0.7414$</td>
<td>$R^2 = 0.7414$</td>
<td>$R^2 = 0.7685$</td>
<td>$R^2 = 0.8126$</td>
</tr>
<tr>
<td>Sm</td>
<td>$y_{60} = 0.0901x + 0.4123$</td>
<td>$y_{70} = 0.0959x + 0.4728$</td>
<td>$y_{80} = 0.1021x + 0.4366$</td>
<td>$y_{90} = 0.1569x + 0.5837$</td>
</tr>
<tr>
<td></td>
<td>$R^2 = 0.7693$</td>
<td>$R^2 = 0.7467$</td>
<td>$R^2 = 0.7955$</td>
<td>$R^2 = 0.8382$</td>
</tr>
</tbody>
</table>

**Second Order Reaction**

Calculation of the second order reaction rate constant required the time-versus $\ln\left(\frac{M - 3X_A}{M - X_A}\right)$ correlation graph. To find the value of M, the number of Y, Nd, Pr and Sm moles in $\frac{M}{M - X_A}$ (1 – $X_A$)

REOH and HNO$_3$ were initially calculated.

$M = \text{mol HNO}_3 \times \text{C}_{(B0)} / \text{mol C}_{(A0)}$ (Y, Nd, Pr and Sm) hydroxide

Mol HNO$_3$ = 0.0576 and moles Y, Nd, Pr and Sm are seen in Table 3. Table 3 presents the M values for Y, Nd, Pr and Sm elements.

**Table 3.** M value for Y, Nd, Pr and Sm

<table>
<thead>
<tr>
<th>Element</th>
<th>M Y</th>
<th>M Pr</th>
<th>M Nd</th>
<th>M Sm</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>9.5624</td>
<td>19.056</td>
<td>4.01</td>
<td>6.5559</td>
</tr>
</tbody>
</table>

The results of second order reaction could be seen in Figures 3a–3d and Table 4.
Figure 3c. Correlation between time and \( \frac{\ln (M - 3X_A)}{M(1 - X_A)} \) for determining k value linearity of second order of Pr element.

Figure 3d. Correlation between time and \( \frac{\ln (M - 3X_A)}{M(1 - X_A)} \) for determining k value linearity of second order of Sm element.

The linear regression value obtained from the square root of \( R^2 \) in the second order reaction of elements Y, Nd, Pr and Sm at various temperatures was presented in Table 4.

Table 4. The equation and the value of linearity (\( R^2 \)) in the second order reaction

<table>
<thead>
<tr>
<th>Element</th>
<th>Temperature, °C</th>
<th>( y ) = ( ax + b )</th>
<th>( R^2 )</th>
<th>( -\ln k )</th>
</tr>
</thead>
<tbody>
<tr>
<td>Y</td>
<td>60</td>
<td>0.0791x + 0.3636</td>
<td>0.7463</td>
<td>2.537</td>
</tr>
<tr>
<td></td>
<td>70</td>
<td>0.0868x + 0.4</td>
<td>0.7637</td>
<td>2.537</td>
</tr>
<tr>
<td></td>
<td>80</td>
<td>0.1132x + 0.495</td>
<td>0.7837</td>
<td>2.537</td>
</tr>
<tr>
<td></td>
<td>90</td>
<td>0.1578x + 0.5976</td>
<td>0.8365</td>
<td>2.537</td>
</tr>
<tr>
<td>Nd</td>
<td>60</td>
<td>0.0936x + 0.4124</td>
<td>0.7892</td>
<td>2.537</td>
</tr>
<tr>
<td></td>
<td>70</td>
<td>0.1011x + 0.4296</td>
<td>0.8001</td>
<td>2.537</td>
</tr>
<tr>
<td></td>
<td>80</td>
<td>0.1289x + 0.4641</td>
<td>0.8456</td>
<td>2.537</td>
</tr>
<tr>
<td></td>
<td>90</td>
<td>0.2007x + 0.6357</td>
<td>0.8638</td>
<td>2.537</td>
</tr>
<tr>
<td>Pr</td>
<td>60</td>
<td>0.0794x + 0.4217</td>
<td>0.7052</td>
<td>2.537</td>
</tr>
<tr>
<td></td>
<td>70</td>
<td>0.0864x + 0.478</td>
<td>0.7451</td>
<td>2.537</td>
</tr>
<tr>
<td></td>
<td>80</td>
<td>0.1033x + 0.457</td>
<td>0.7723</td>
<td>2.537</td>
</tr>
<tr>
<td></td>
<td>90</td>
<td>0.146x + 0.5717</td>
<td>0.8167</td>
<td>2.537</td>
</tr>
<tr>
<td>Sm</td>
<td>60</td>
<td>0.0833x + 0.366</td>
<td>0.7587</td>
<td>2.537</td>
</tr>
<tr>
<td></td>
<td>70</td>
<td>0.0889x + 0.423</td>
<td>0.7587</td>
<td>2.537</td>
</tr>
<tr>
<td></td>
<td>80</td>
<td>0.0949x + 0.3883</td>
<td>0.808</td>
<td>2.537</td>
</tr>
<tr>
<td></td>
<td>90</td>
<td>0.1489x + 0.5256</td>
<td>0.8509</td>
<td>2.537</td>
</tr>
</tbody>
</table>

Linearity values (\( R^2 \)) of first order reaction (Table 2) were smaller compared to the linearity values (\( R^2 \)) second order reaction (Table 4), so it could be stated that the reaction was second order.

In general, the determinant of the reaction rate was the phase with the smallest rate, especially for the chemical reactor design [30].

The list of k values of the 2\(^{nd}\) order reaction at various temperatures can be arranged in Table 5.

Table 5. The k values of 2\(^{nd}\) order reaction at various temperature

<table>
<thead>
<tr>
<th>Temperature, °C</th>
<th>T, °K</th>
<th>k, liter/mole.time</th>
<th>1/T</th>
<th>ln k</th>
<th>- ln k</th>
</tr>
</thead>
<tbody>
<tr>
<td>Y</td>
<td>60</td>
<td>333</td>
<td>0.0791</td>
<td>0.0030</td>
<td>-2.537</td>
</tr>
<tr>
<td></td>
<td>70</td>
<td>343</td>
<td>0.0868</td>
<td>0.0029</td>
<td>-2.444</td>
</tr>
<tr>
<td></td>
<td>80</td>
<td>353</td>
<td>0.1132</td>
<td>0.0028</td>
<td>-2.179</td>
</tr>
<tr>
<td></td>
<td>90</td>
<td>363</td>
<td>0.1578</td>
<td>0.0028</td>
<td>-1.846</td>
</tr>
<tr>
<td>Pr</td>
<td>60</td>
<td>333</td>
<td>0.0794</td>
<td>0.0030</td>
<td>-2.533</td>
</tr>
<tr>
<td></td>
<td>70</td>
<td>343</td>
<td>0.0868</td>
<td>0.0029</td>
<td>-2.444</td>
</tr>
<tr>
<td></td>
<td>80</td>
<td>353</td>
<td>0.1132</td>
<td>0.0028</td>
<td>-2.179</td>
</tr>
<tr>
<td></td>
<td>90</td>
<td>363</td>
<td>0.1578</td>
<td>0.0028</td>
<td>-1.846</td>
</tr>
</tbody>
</table>
After obtaining the element’s reaction rate constants of second order reaction at each temperature, the correlation of the reaction rate constant $k$ as a function of temperature by referring to the Arrhenius equation, $\ln k = \ln A - \frac{E_a}{R T}$. (equation 15).

The calculation results are expressed in the linear line graph between $\ln k$ as ordinate and $1 / T$ as the abscissa for Y, Nd, Pr and Sm element could be observed in Figure 4. From Figure 4, the relationship between $1 / T$ and $\ln k$, line alignment was expressed by $R^2$, the slope obtained was the activation energy and the intercept was the frequency factor.

![Figure 4a. Correlation between 1/T and -ln k for Y, Pr, Nd and Sm element](image)

The linear equation of the correlation between $1 / T$ (x) and $-\ln K$ (y) could be seen in Table 6. The activation energy was defined as the energy that must be exceeded so that chemical reactions can occur. Frequency factor (A) depends on the weight and molecular structure, frequency and position of collisions between molecules. The value of the frequency factor (A) could be determined from the intercept and the activation energy (E) was the value of the slope multiplied by $R$ (gas constant 8.314 J/mole°K). The calculation results of A and E values could be observed also in Table 6. From Table 6 it could be seen that the largest activation energy was Y of 23.34 kJ/mole followed by Pr of 20.00 kJ/mole. Sm of 17.94 kJ/mole and the smallest one was Nd of 16.39 kJ/mole.
Ferdowsi et al. did and optimizing and kinetics of leaching process of cerium, lanthanum and neodymium elements of apatite using nitric acid. The maximum leaching efficiency of which were 66.1%, 56.8% and 51.7% respectively for Ce, La and Nd, achieved under the optimum leaching conditions with nitric acid concentration of 18%, 0.06 ratio of solid to liquid and leaching time of 38 minutes, the activation energy of Ce of 6.54 kJ / mole[20]

### 5. Conclusion
The leaching process was strongly influenced by the temperature and time of process. Leaching of REOH using nitric acid follows second order reaction. In leaching 10 g of REOH using 40 ml of HNO₃ 0.0576 moles were obtained maximum conversion at 90 °C and leaching time of 15 minutes for Y was 0.95 (leaching efficiency of 95%). for Nd was 0.97 (leaching efficiency of 97%). for Pr was 0.94 (leaching efficiency of 94%) and for Sm was 0.94 (leaching efficiency of 94%). The largest activation energy was Y of 23.34 kJ / mole followed by Pr of 20.00 kJ/mole, Sm of 17.94 kJ / mole and the smallest was Nd of 16.39 kJ / mole. The correlation between the reaction rate constant with T for Y was kY = 338.26 e⁻¹²·³₄ / RT, for Nd was kNd = 33.69 e⁻¹⁶·₃₉ / RT, for Pr was kPr = 102.04 e⁻¹⁰ / RT and for Sm was kSm = 50.16 e⁻¹⁷·₉₄ / RT

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